

ÉTUDE DE LA DISSOLUTION DE L'HYDROGÈNE DANS LA SAUMURE DANS LE CADRE DU STOCKAGE EN NAPPE AQUIFÈRE



Chaire junior HYDR

Lancée en avril 2021

Durée : 5 ans

Dr. Salaheddine CHABAB

Pr. Pierre CÉZAC

Pr. Guillaume GALLIERO

Halla KERKACHE (PhD student)

Dr. Marion DUCOUSSO

Dr. Marie POULAIN

Post-doc (bientôt)



Scope

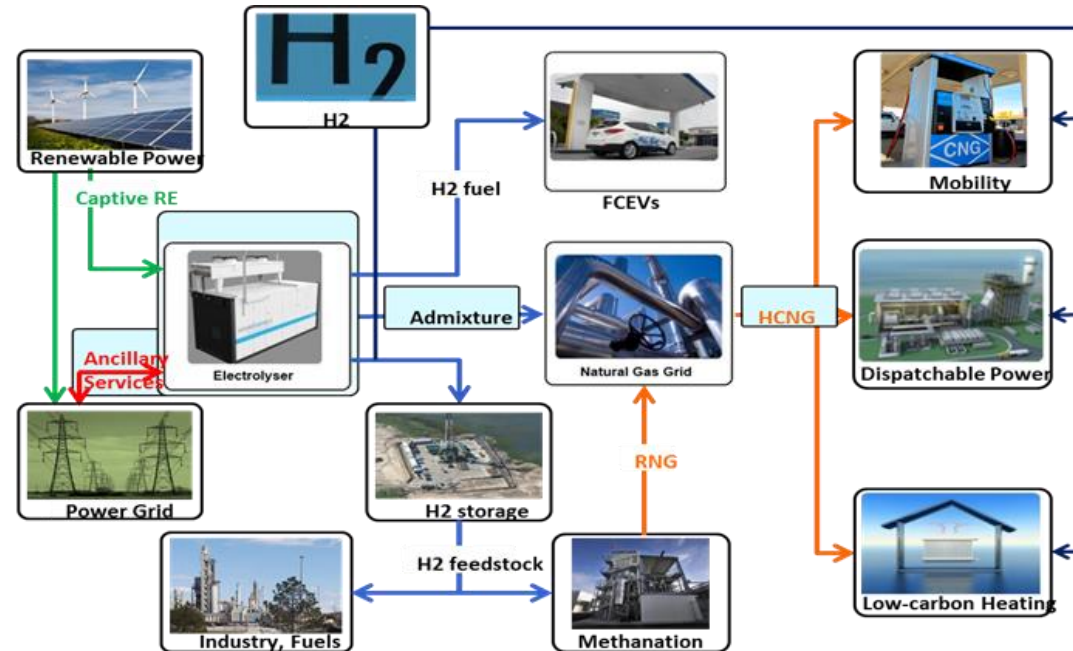
- ✓ H₂ (+ NG and/or CO₂) mobility in Aquifers
- ✓ H₂ Storage, Natural H₂ exploration, and Geothermal energy

Framework (E2S)

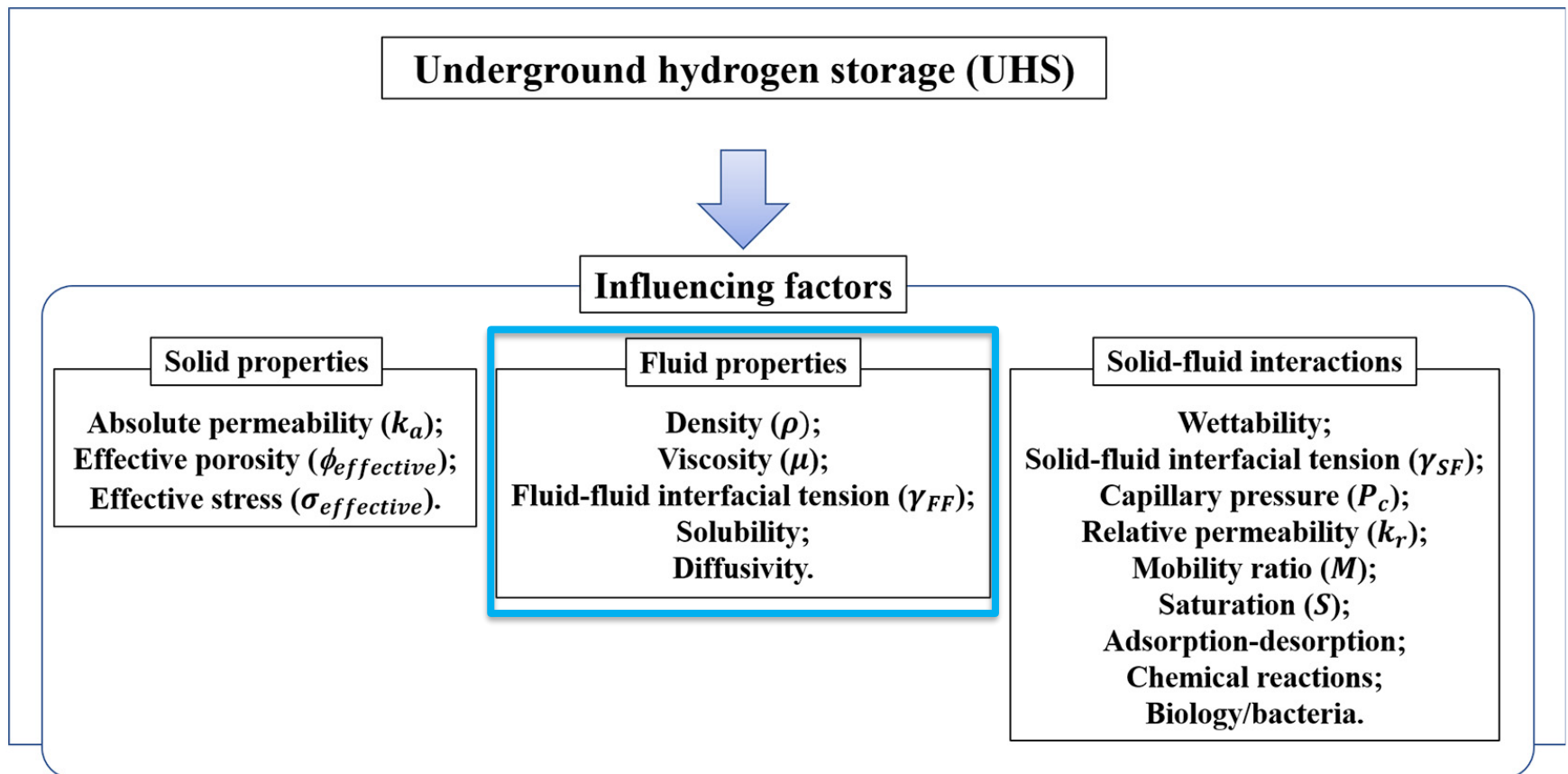
- ✓ HYDR Junior Chair (S. Chabab)
- ✓ Exps + Mol Sim + EoS Models
- ✓ LFCR + LATEP + ProSim + IFPEN

Activities/Projects

- PhD (2021-2024, H. KERKACHE): Solubility + Diffusion in brine and clay. Mol Sim + exps
- PDRA (2022-2024, ProSim): Advanced Modeling
- Implementation in ProSim Tools

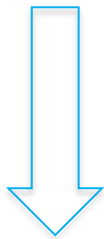


Multi-scale parameters relevant in Underground Hydrogen Storage

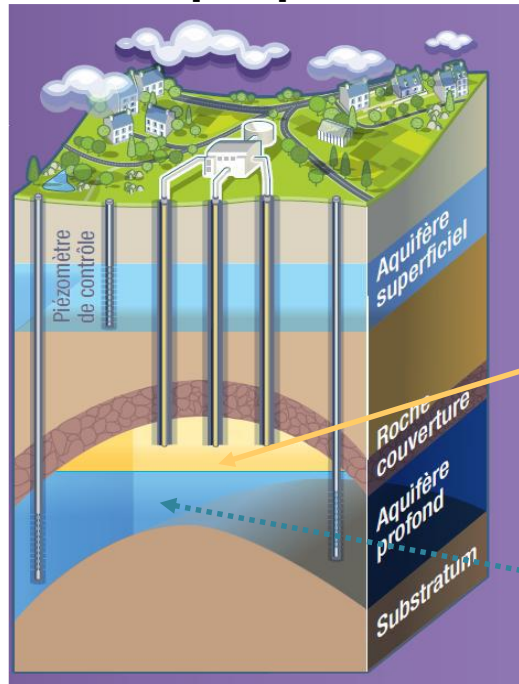


Fluid properties

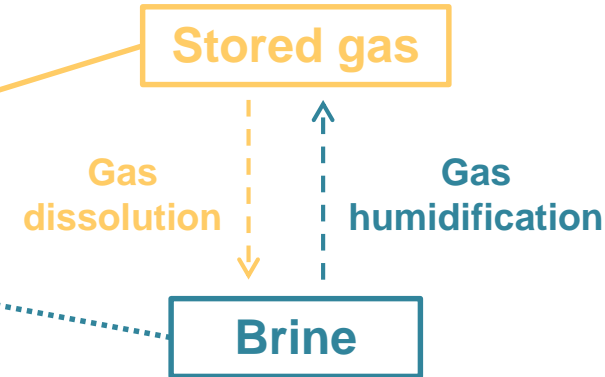
- ❖ Gas solubility
- ❖ Water content in gas phase
- ❖ Diffusion coefficient
- ❖ IFT (MS)



Deep aquifers



Ref : INERIS



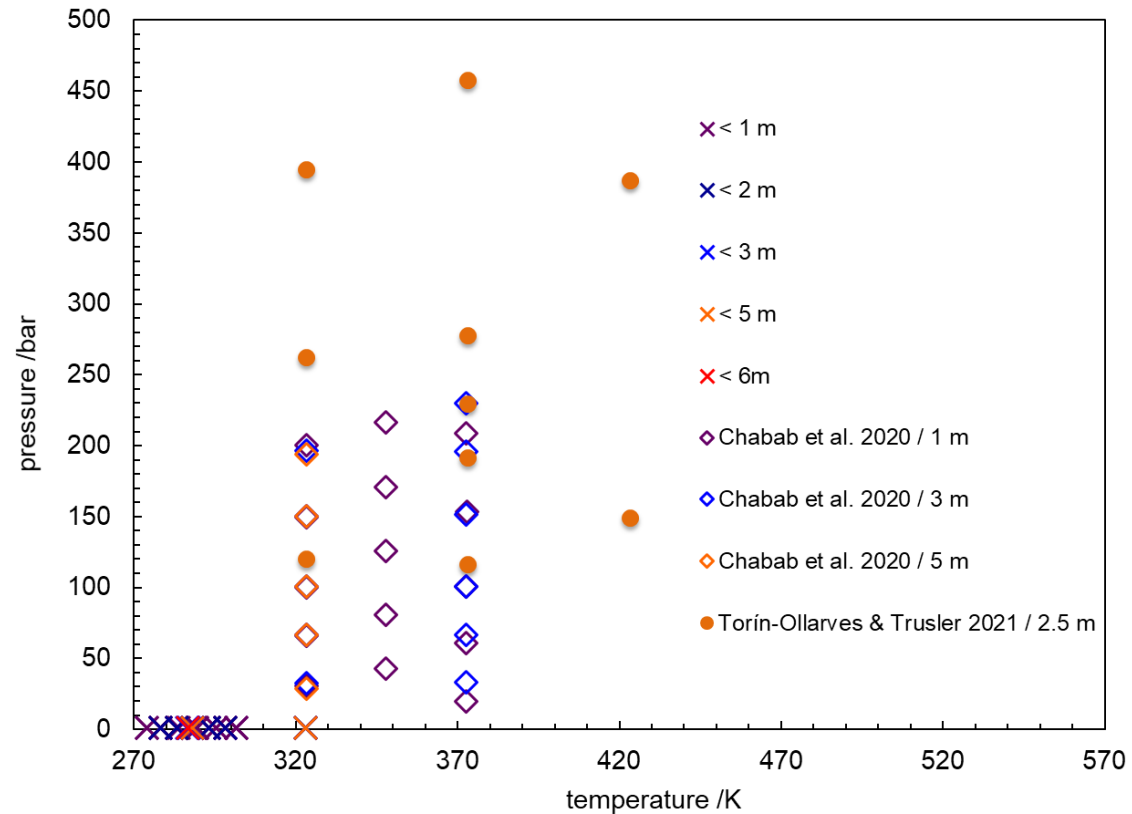
- ➔ Estimation of storage capacities and losses by dissolution
- ➔ Design / Simulation of surface facilities (e.g. gas dehydration after withdrawal)
- ➔ Gas reactivity study
- ➔ Estimate the amount of cushion gas



- Only 2 experimental studies ($P > P_{\text{atm}}$) :
 - [Chabab et al. 2020](#) (**capillary sampling + GC** at known T/P)
 - [Torín-Ollarves & Trusler 2021](#) (**bubble-point** pressure at known T/x)
- 1 MS study: Lopez-Lazaro et al. 2019

- **Large deviations** (up to **30%**) between the reported data

=> **Interest** to conduct **more studies: Experimental and Molecular Simulation !**

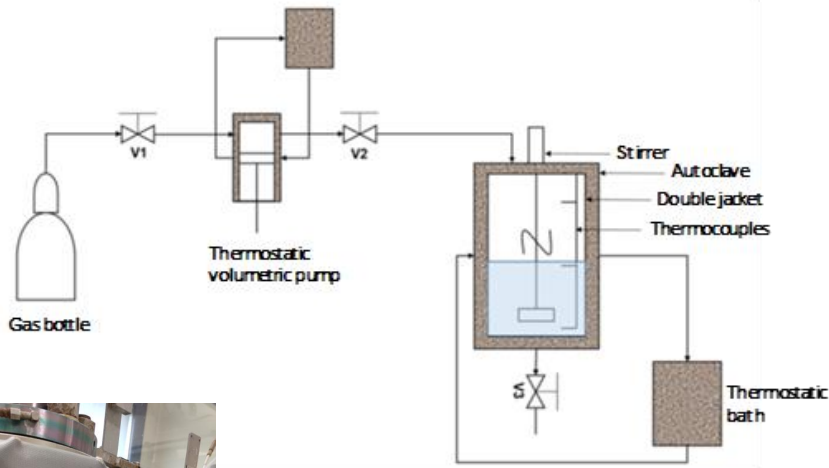


Apparatus for measuring gas
solubility in liquids: **presentation**
and **validation** of the **protocol**



Laboratory tests (LaTEP lab)

Protocol development and validation



Phase equilibrium part

Potentiometric titration

Analysis part



Equilibrium Cell

Adaptation of an existing apparatus

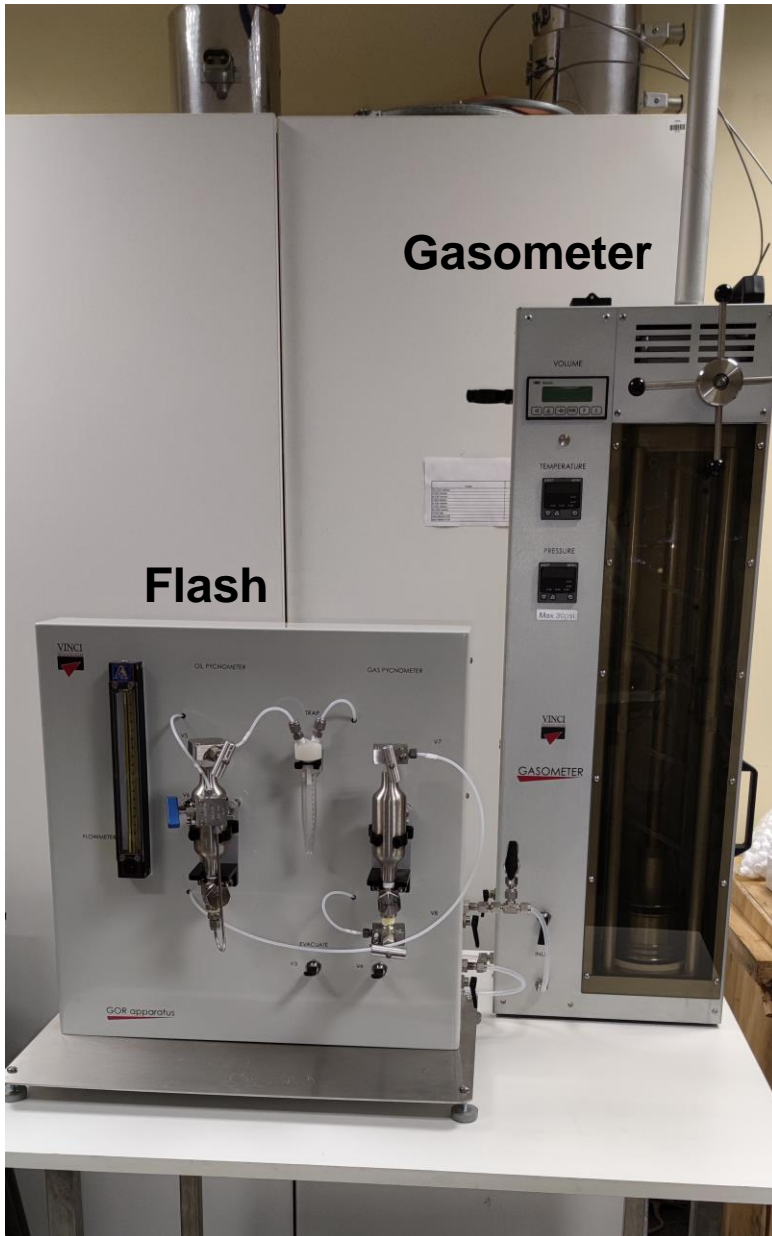
- Old analytical technique : potentiometric titration
- New analytical technique : **Volumetric & gravimetric**
- Verification of pressure equipment
- Change of fluid : Change from a "Group 2 gas" fluid to a "**Group 1 gas**" fluid



Flash

Gasometer

Sample collection in the Flash pycnometer



+ GC (if gas mixture)



Sample collection in the Flash pycnometer



Sampling and analysis



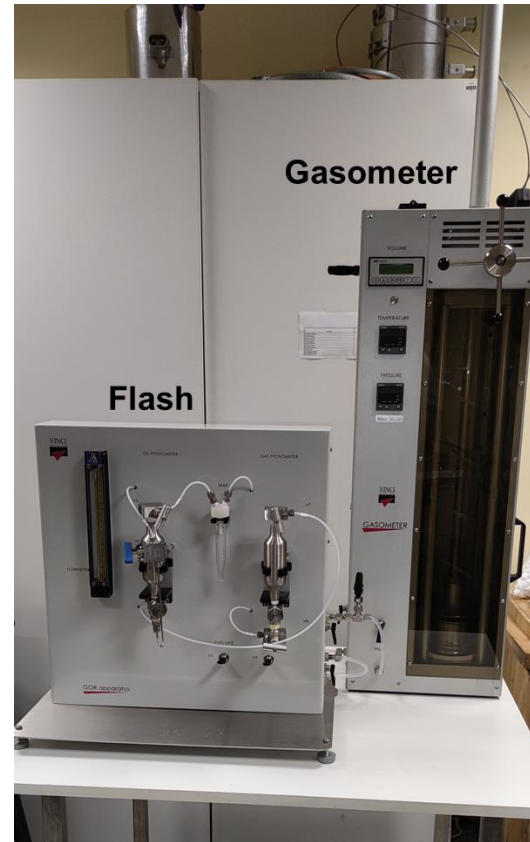
m_0



Sampling



m_1



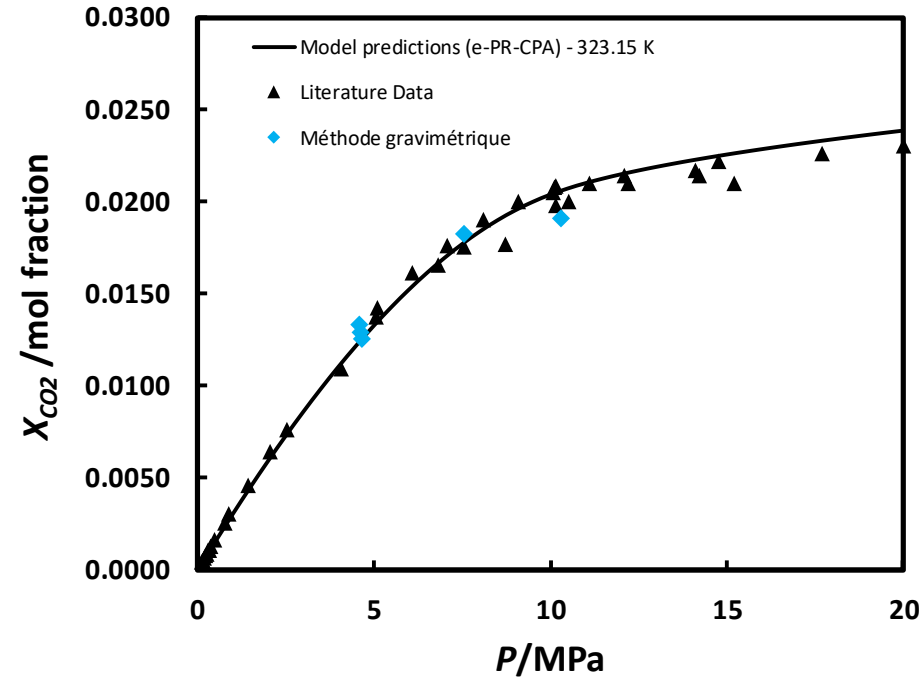
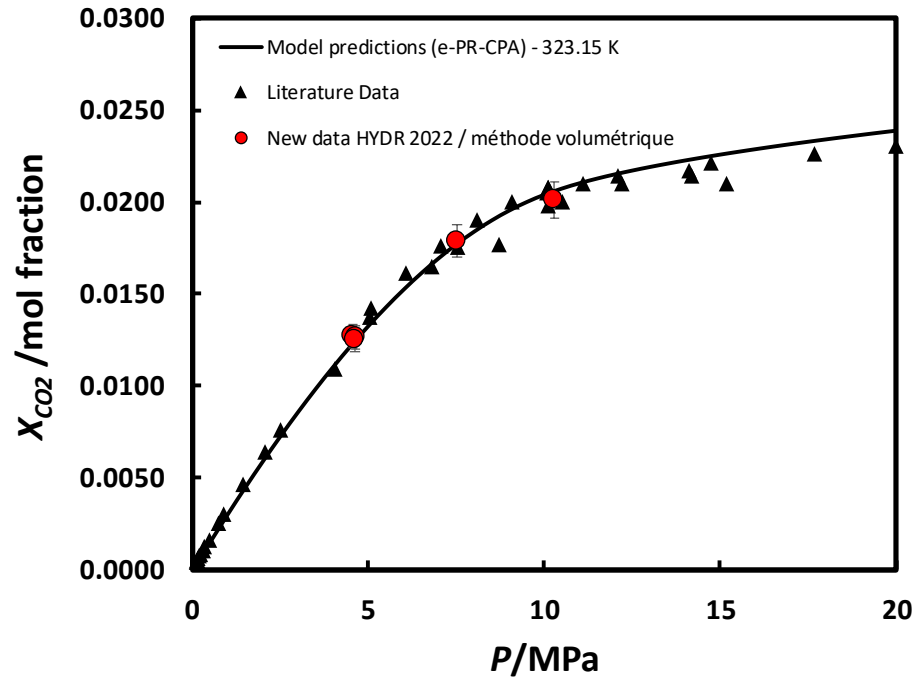
Degassing



m_2



New data vs Literature data (for validation purpose)



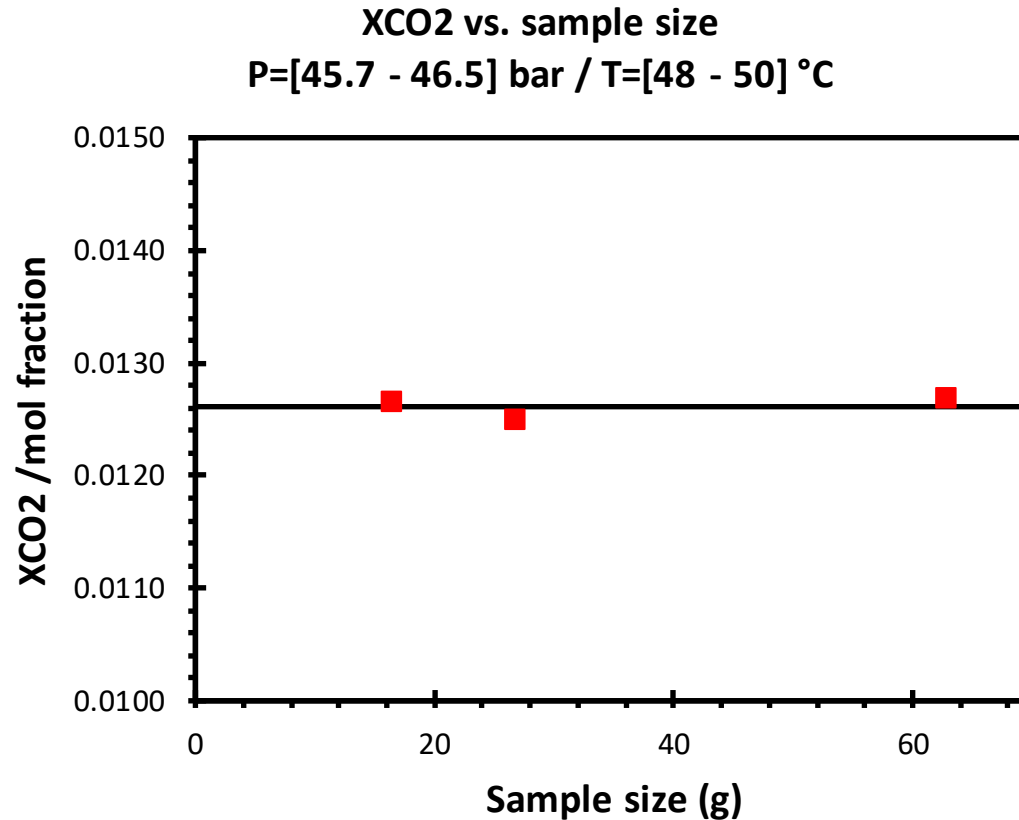
Method 1 : Volumetric determination

Method 2 : Gravimetric determination

	P (MPa)	T (K)	GLR (Nm ³ /m ³)	Sample size (g)	m _{Gas} (g)
Pt1	4.57	321.55	15.81	62.85	1.96
Pt2	4.65	323.45	15.71	16.40	0.48
Pt3	4.63	323.45	15.65	26.82	0.81
Pt4	7.53	323.15	22.95	36.15	1.58
Pt5	10.30	324.75	26.13	10.47	0.48

Repeatability /
reproducibility check





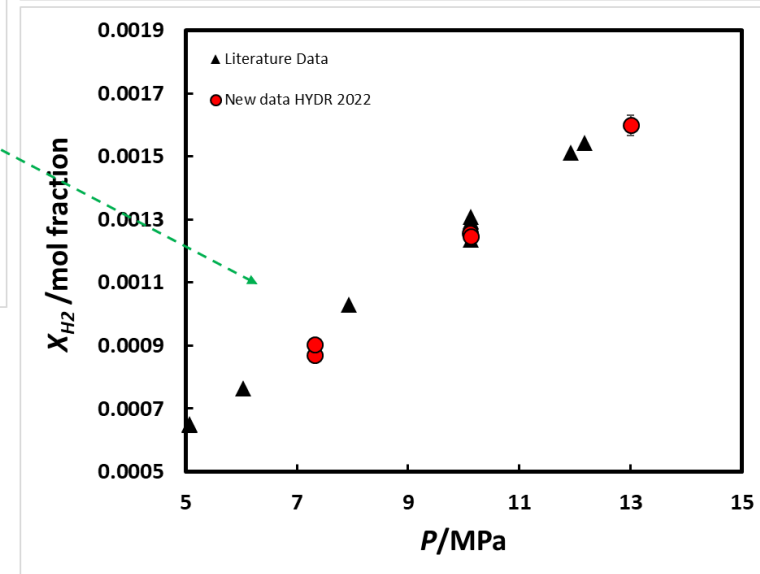
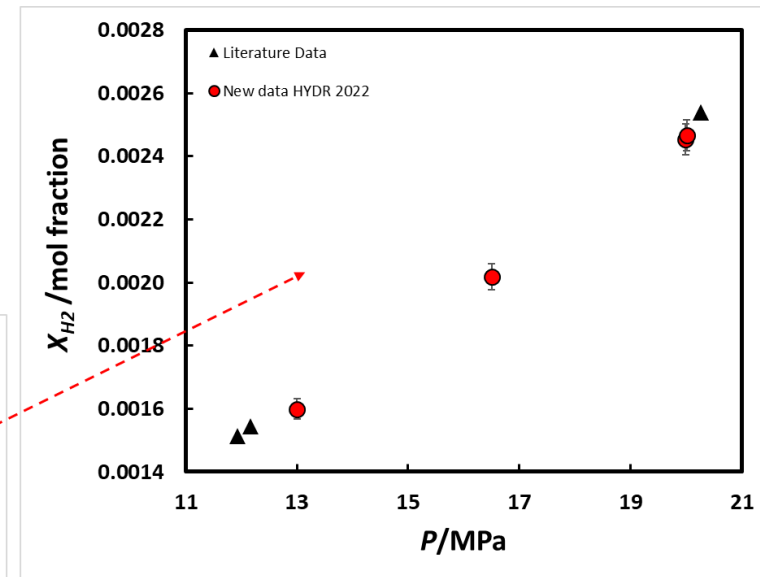
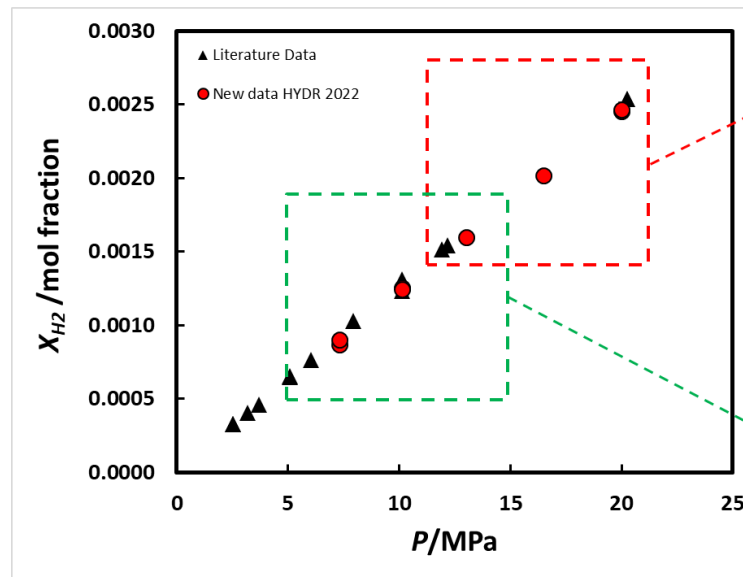
Verification of the non-dependence on the sample size

Measuring the H₂ dissolution in water and brine



Measurements of H₂ solubility in pure H₂O:

→ 8 equilibrium points at 50° C (7 – 20 MPa)

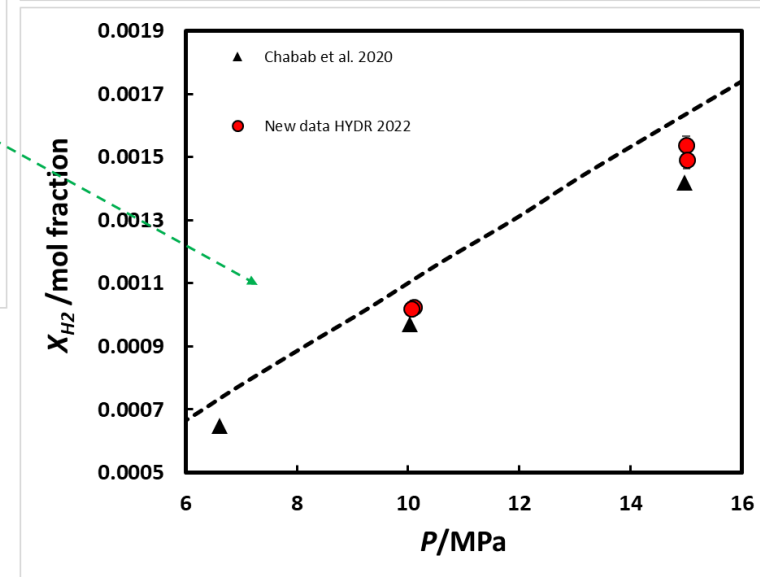
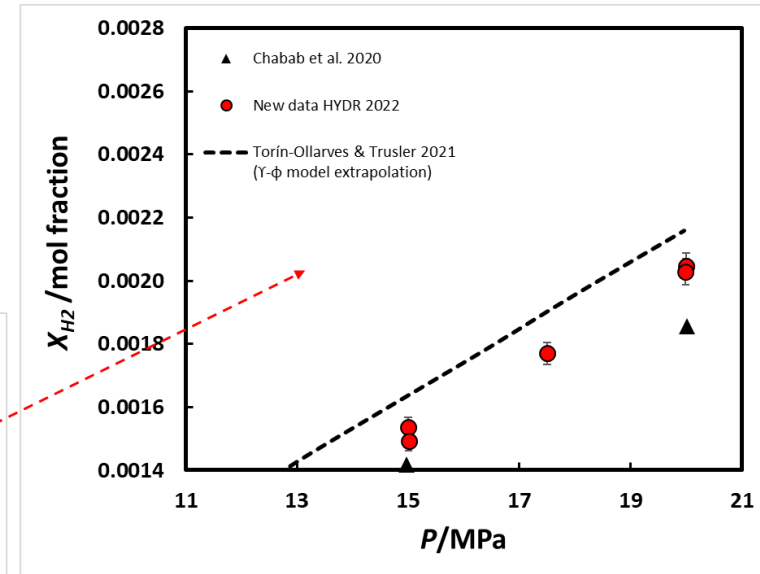
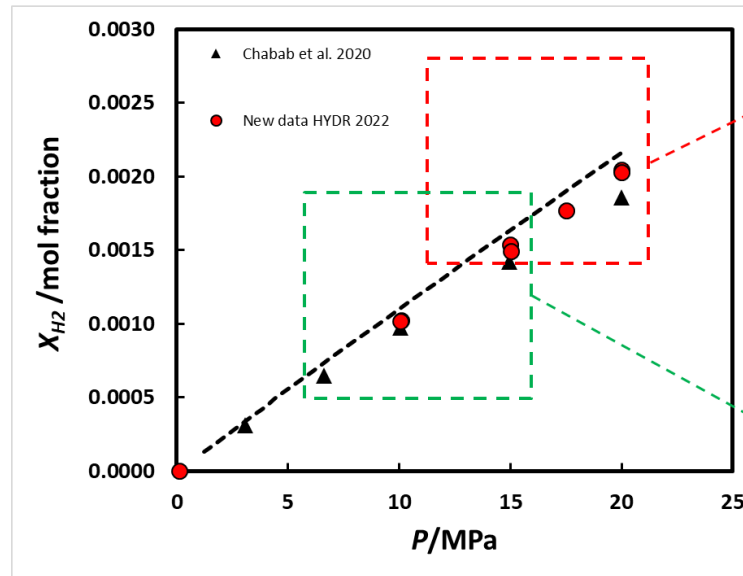


□ Results **consistent** with literature data

□ Due to the **low H₂ solubility**, measurements are **easier** at **high-pressure** (better repeatability and less uncertainty)

Measurements of H₂ solubility in 1m NaCl brine:

→ 8 equilibrium points at 50° C (10 – 20 MPa)



❑ Closer to Torín-Ollarves & Trusler 2021 than Chabab et al. 2020 data

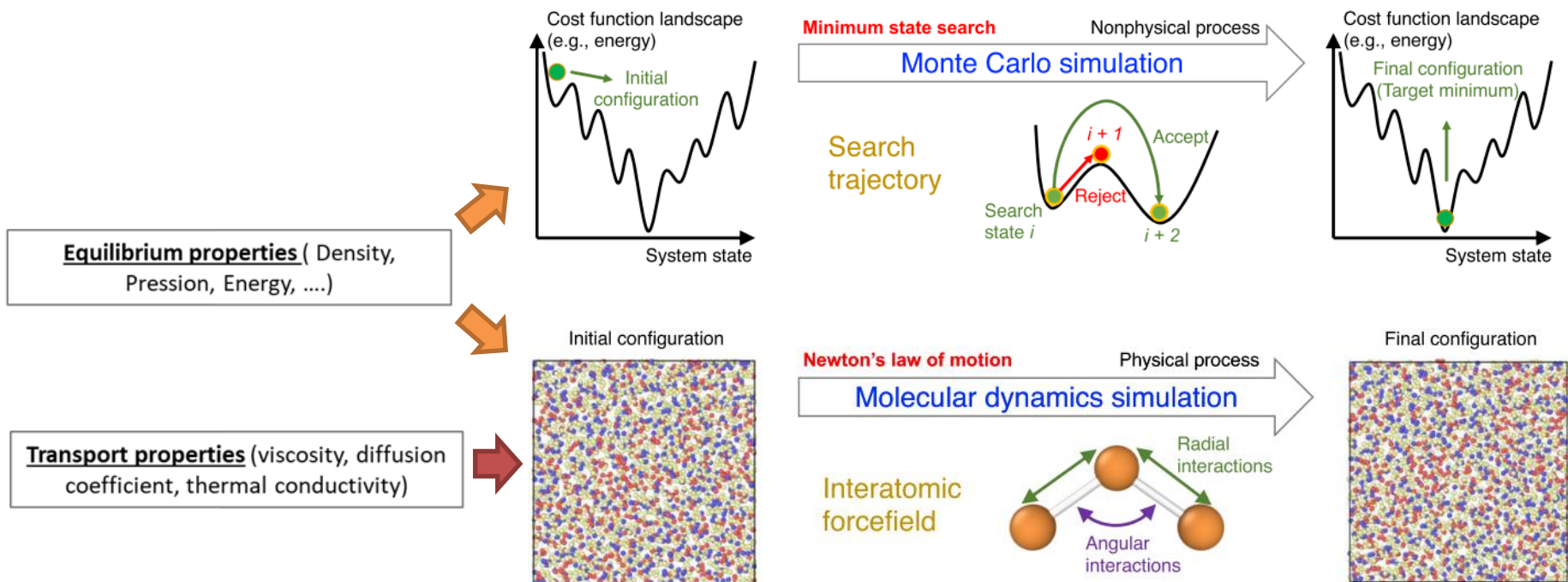
❑ Torín-Ollarves & Trusler 2021 and this work expect a **lower salting-out** than that reported by Chabab et al. 2020

Studying the H₂ solubility using
Monte Carlo simulation



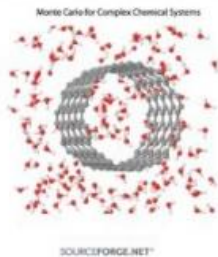
WHAT IS AND WHY MOLECULAR SIMULATION?

- High-performance computing (HPC)
- Force field
- Statistical method (Monte Carlo)
- Newton's law of motion (Molecular Dynamics)

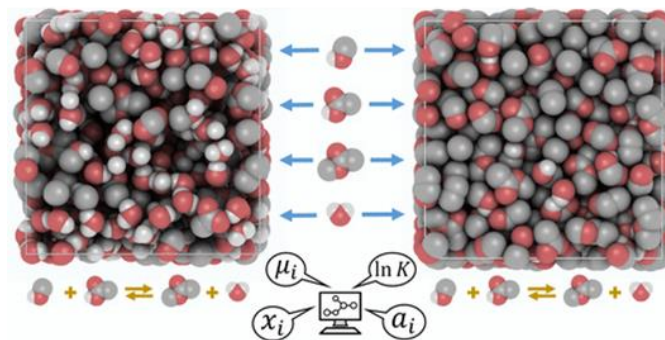


- 2 tools are used for the calculation of H_2 solubility by performing Monte Carlo simulations : **Towhee** and **Brick-CFCMC**

MCCCS Towhee



Brick-CFCMC



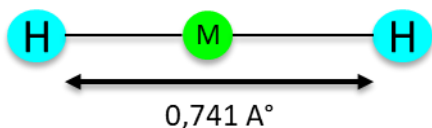
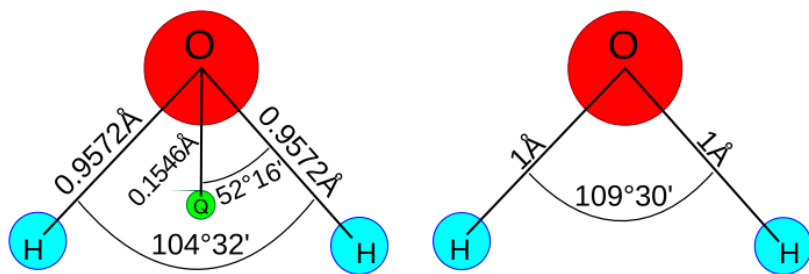
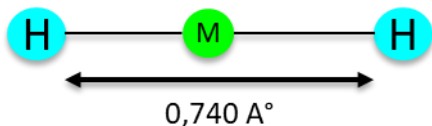
- Model choice :

Pure H_2 model: Alavi, Marx

Pure H_2O model: SPC/E, TIP4P/2005

Binary mixture : Alavi_SPC/E - Alavi2005_TIP4P/2005 - Marx_TIP4P/2005 + Lorentz-Berthelot for mixing rule.

- Use of different methods for the calculation of solubility

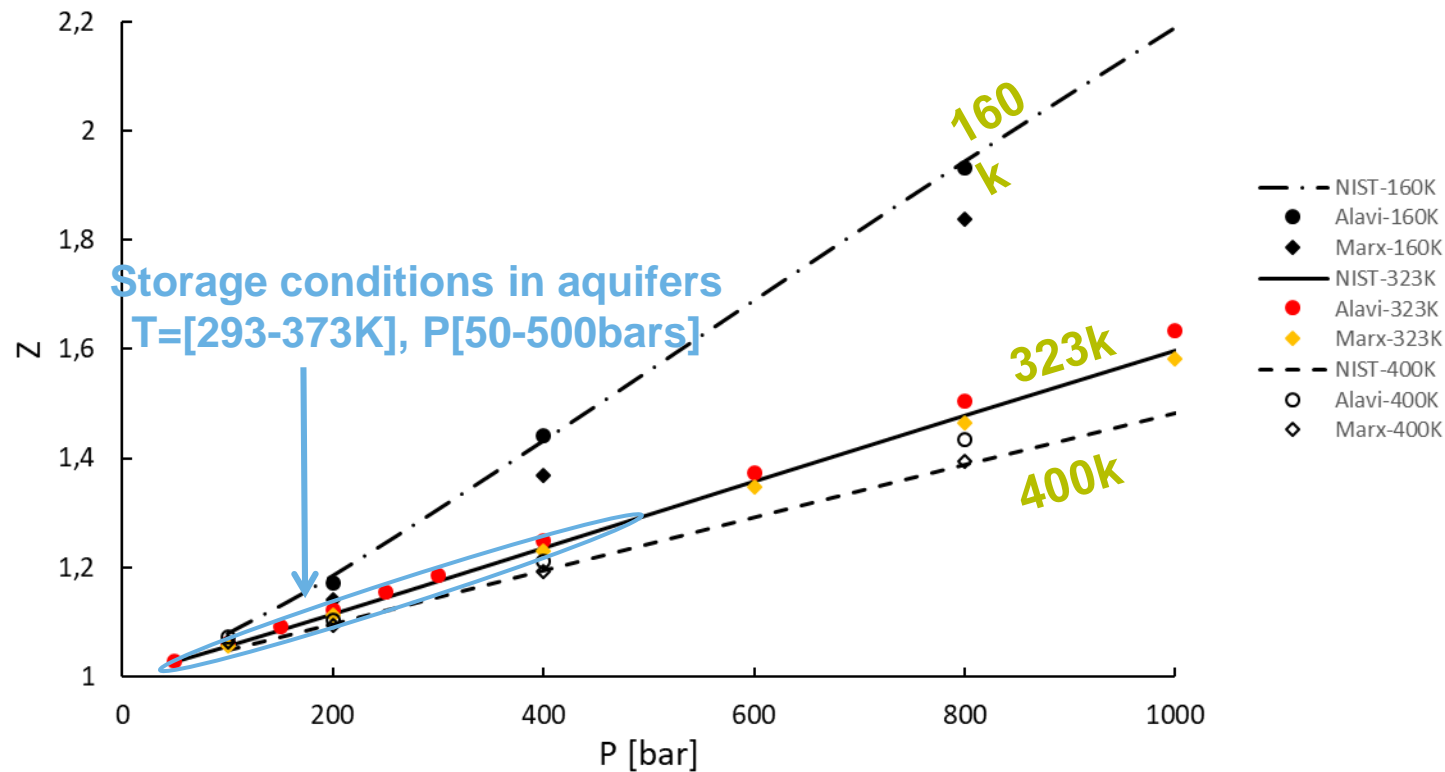
H₂
Alavi 2005

Marx 1992

TIP4P/2005
SPC/E

Ref: Vinš, Václav, et al. "Molecular simulations of the vapor-liquid phase interfaces of pure water modeled with the SPC/E and the TIP4P/2005 molecular models."

Model/atom	q+ (e)	q- (e)	ε (K)	σ (Å°)
Alavi 2005				
H-H ₂	0,4932	-	-	-
M-H ₂	-	-0,9864	34,3	3,038
Marx 1992				
H-H ₂	0,4680	-	-	-
M-H ₂	-	-0,9360	36,7	2,958

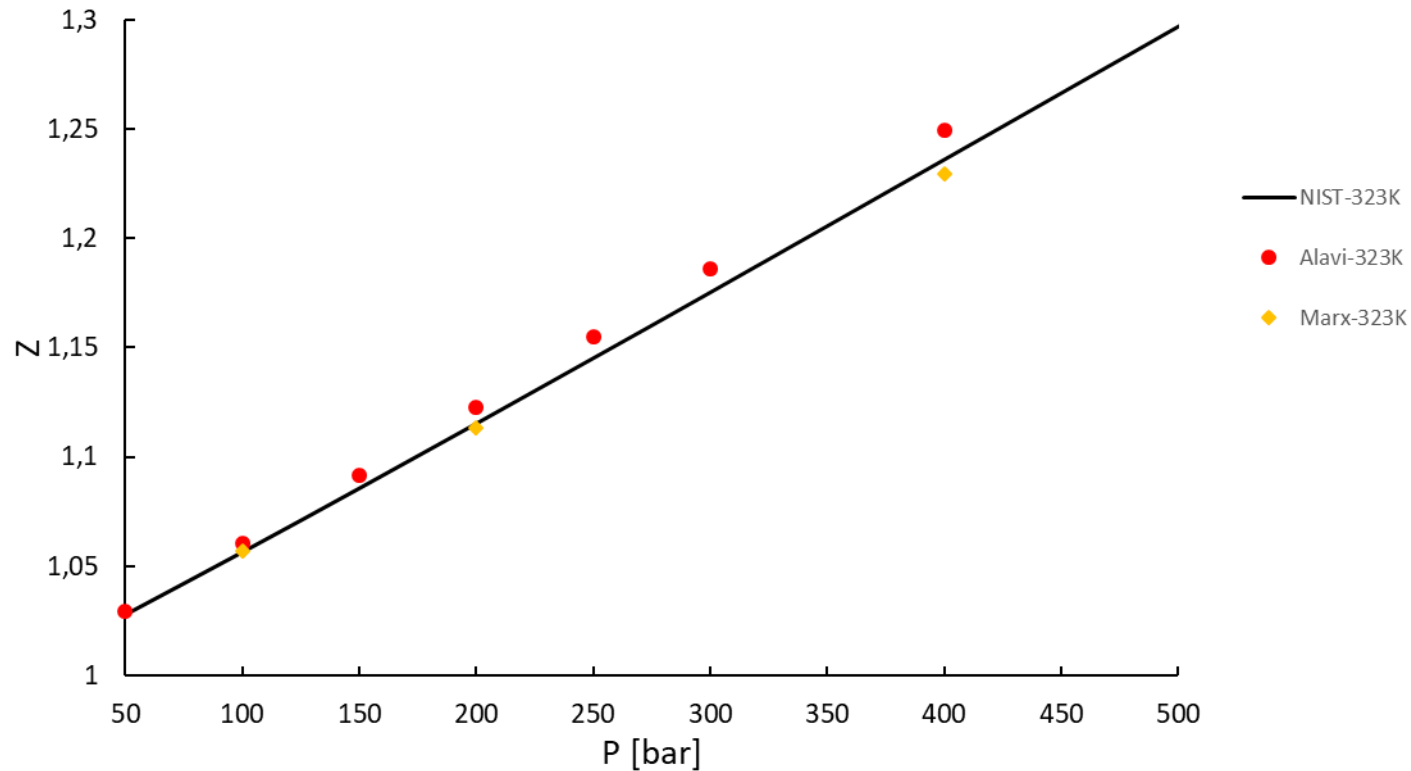
H₂O

Model/atom	q+ (e)	q- (e)	ε (K)	σ (Å°)
SPC/E				
O	-	-0,8476	78,175	3,166
H	0,4932	-	-	-
TIP4P/2005				
O	-	-	93,196	3,1589
H	0,5564	-	-	-
Q	-	-1,1128	-	-



- **At 160K:** Among the two models tested, the Alavi model captures well the compressibility factor ($AAD_{Alavi}=1,5\%$) at low temperature and so the quantum effects.
- **At 400K:** The model of Marx predict well the compressibility factor ($AAD_{Marx}=0,49\%$), However, Alavi is less accurate at high temperature($AAD_{Alavi}=2,17\%$).

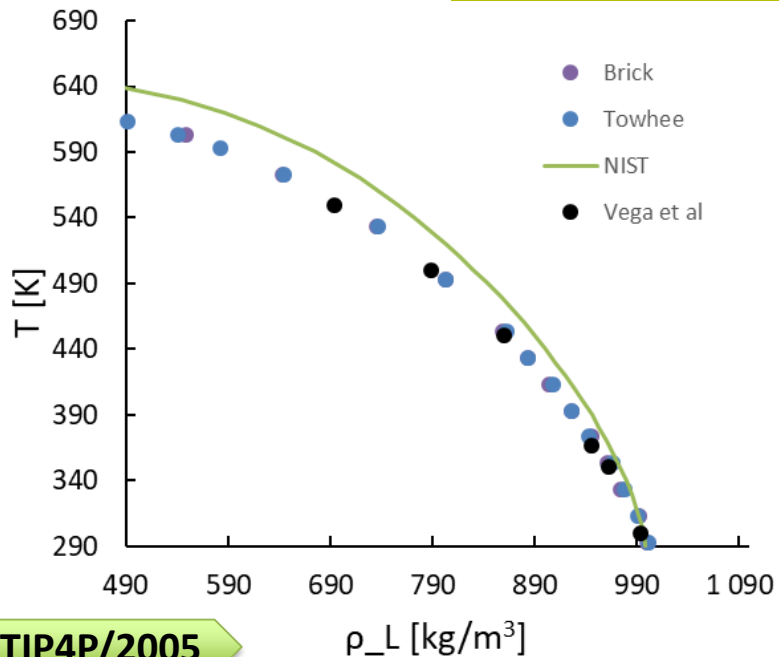




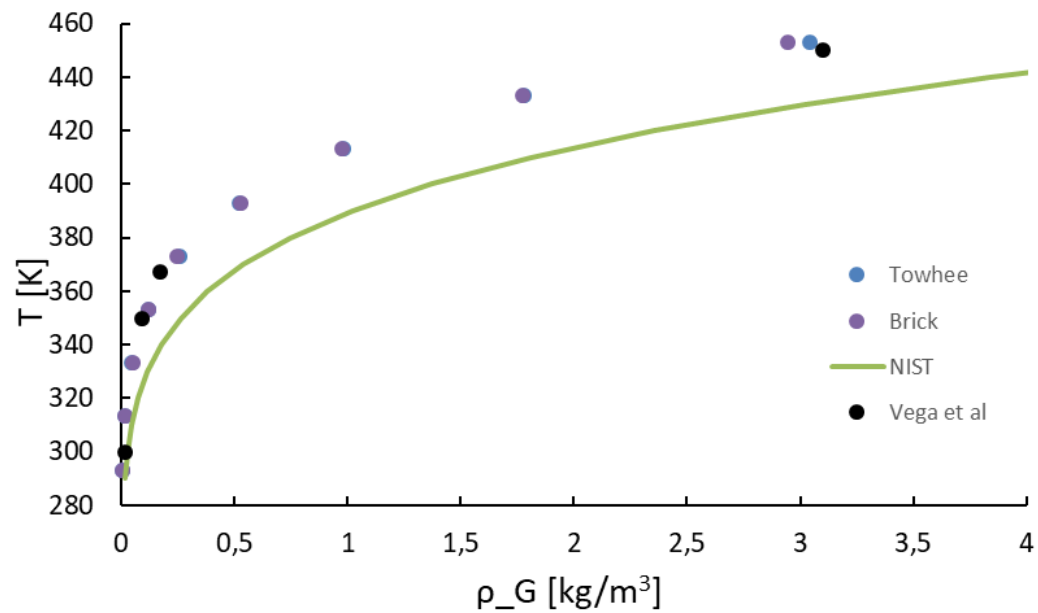
- **At 323K:** all the models predict well the compressibility factor, the AAD obtained are less than 1. (AAD_{Alavi}=0,97%, AAD_{Marx}=0,53%)



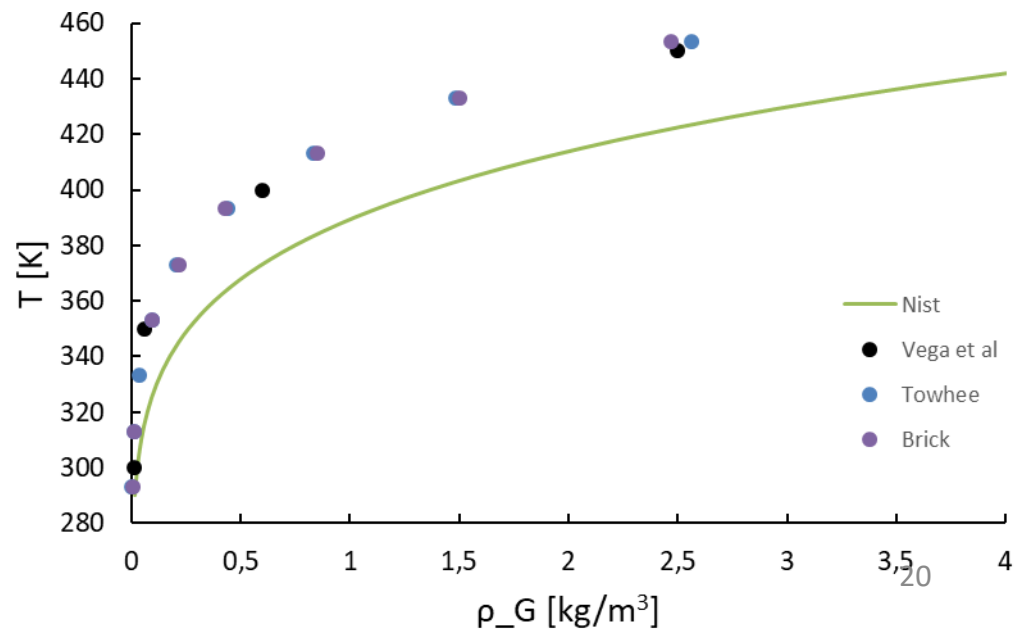
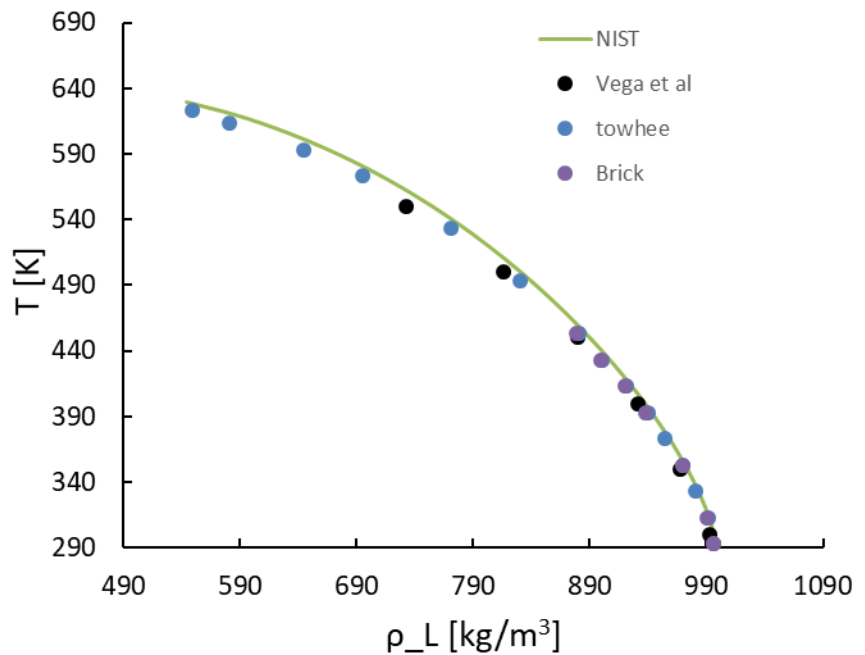
SPC/E



EVALUATION OF FORCE FIELDS : PURE WATER H₂O



TIP4P/2005



- H_i : The solubility of hydrogen in water/brine can be calculated using the **Henry constant**, which is related to the residual chemical potential of the solute i at infinite dilution μ_i^∞ :

$$H_i = \rho k_B T \exp(\mu_i^\infty / k_B T)$$

where k_B is the Boltzmann constant, T the temperature, ρ the density of the solvent.

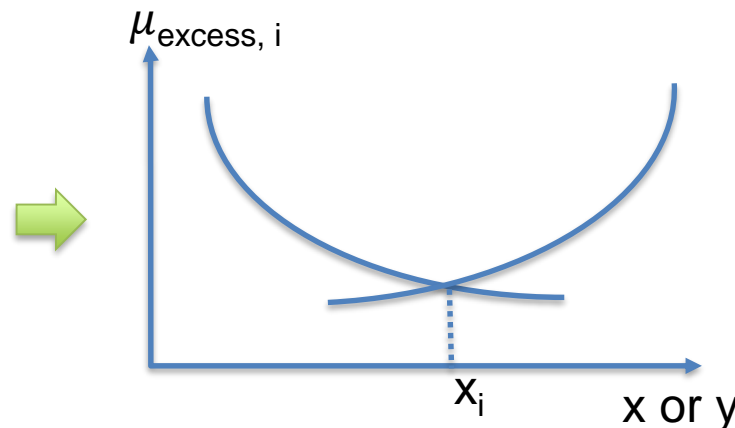
μ_i^∞ : from molecular simulation (MSMC: 1 boxe-NPT ensemble + widom insertion)

- **using Gibbs ensemble** (2boxes -NPT ensemble)
- **Equality of chemical potentials:** NPT simulations => plot the chemical potential as a function of hydrogen composition => the intersection of the two curves (liquid and vapor) represents the solubility of hydrogen at the fixed conditions

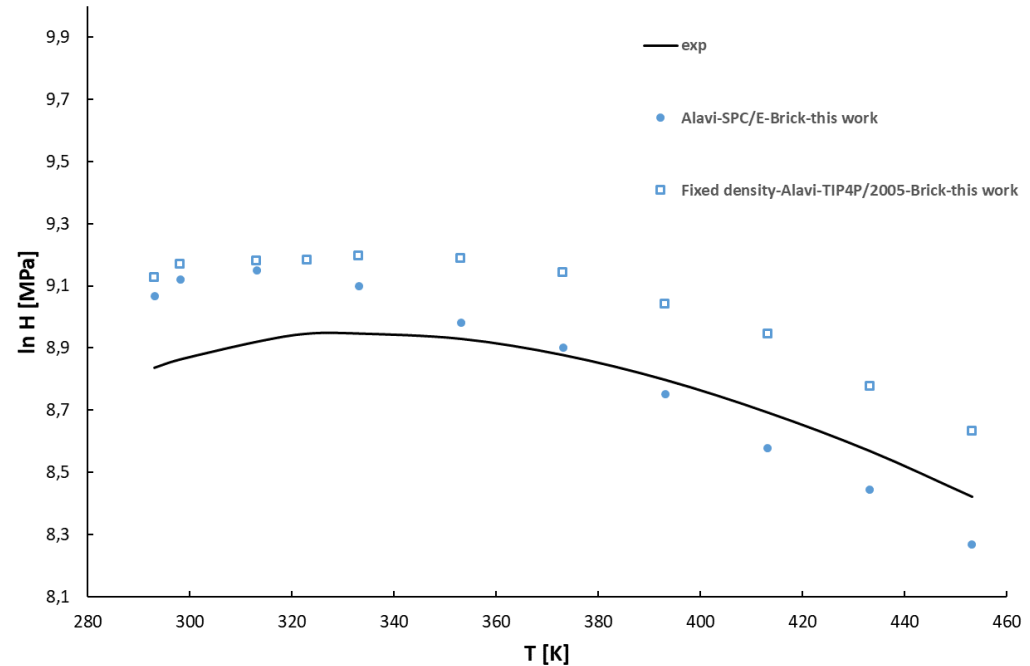
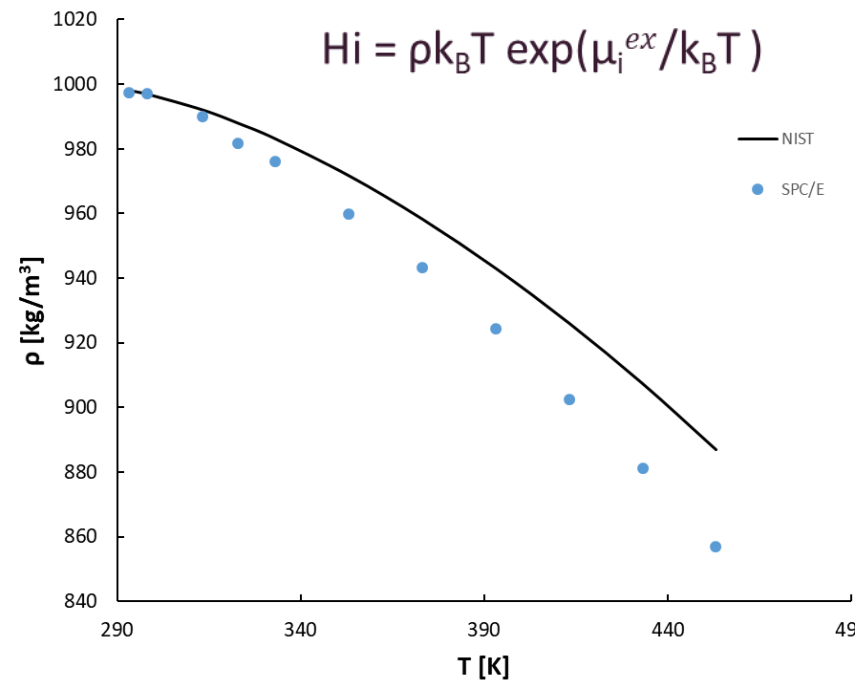
Vapor phase
(H₂+H₂O)
NPT ensembles

Liquid phase
(H₂+H₂O)
NPT ensembles

N simulations	H ₂	H ₂ O	H ₂ O	H ₂
1	600	1	730	1
2	600	2	730	2
3	600	...	730	...
4	600	...	730	...
...



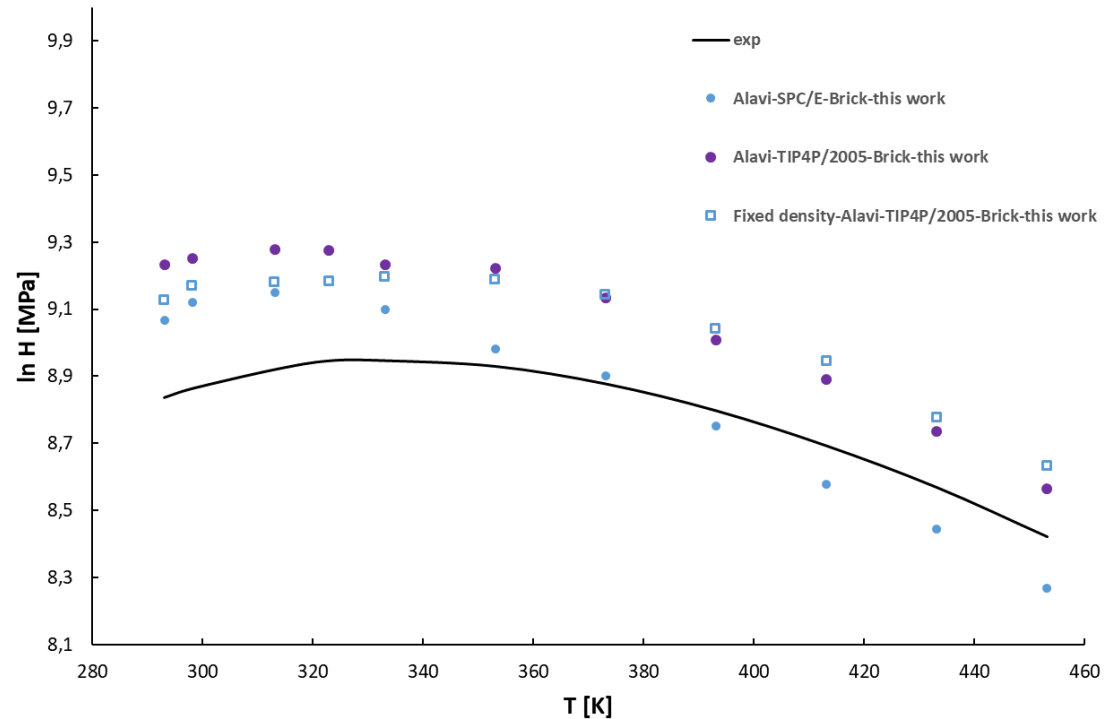
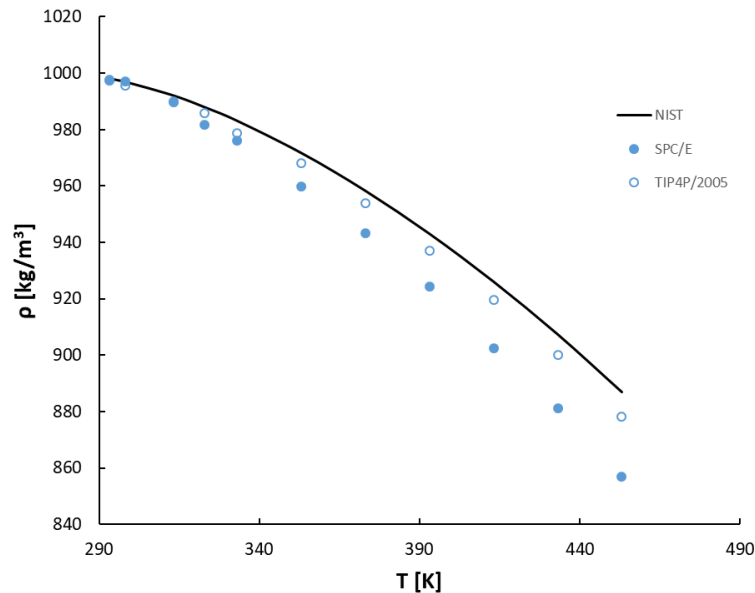
$$\rho = f(T)$$



- At high temperature ($T > 353\text{K}$), the SPC/E model does not capture well the water density => test a new force field for water: **TIP4P/2005**

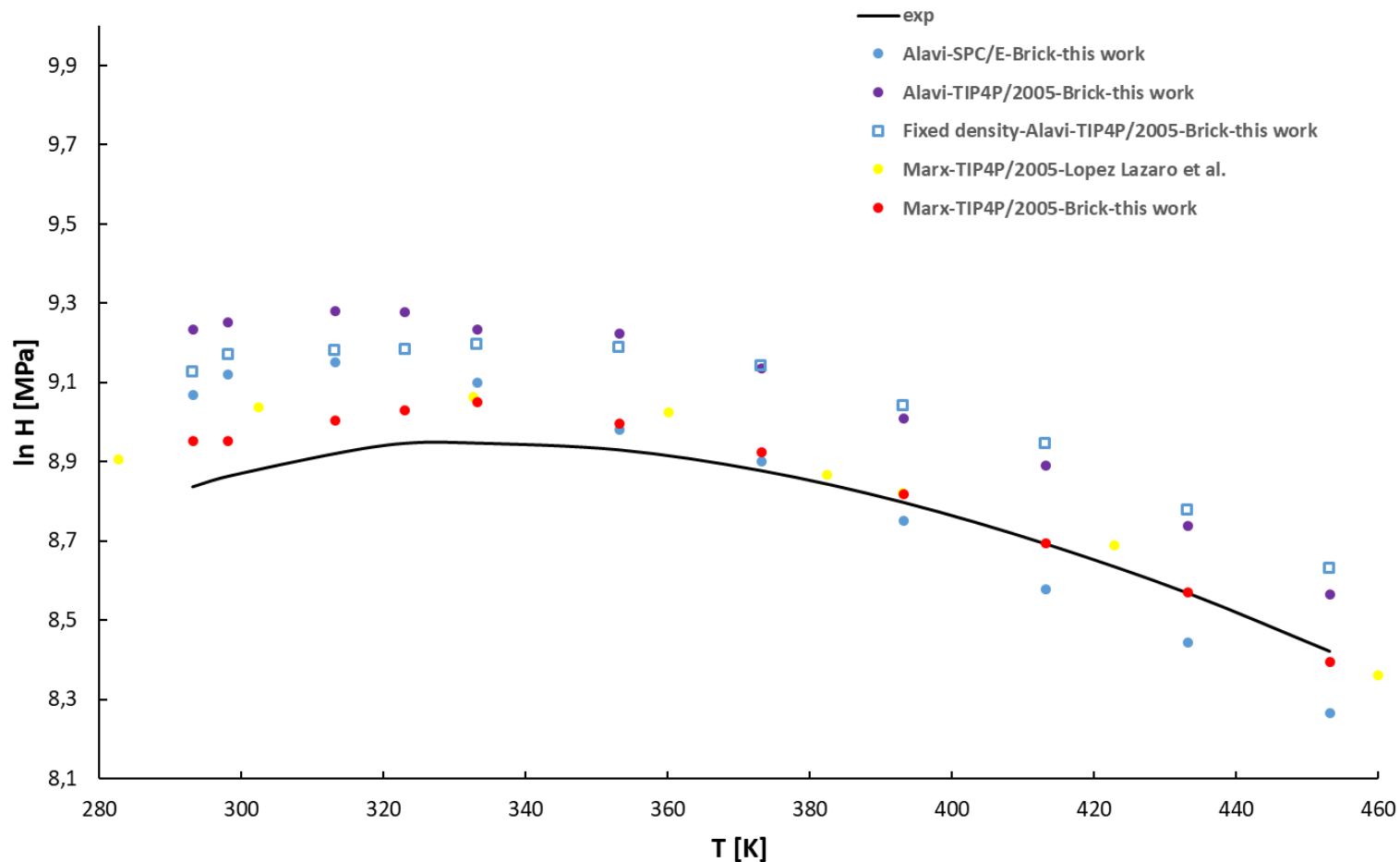


Effect of density on the qualitative representation of H vs. T



By fixing the density (exp) or by using a suitable model for water density (TIP4P/2005), the results are qualitatively much improved (H vs. T)

What can be done to quantitatively improve predictions?



- Using the **Marx** model for H_2 (also used by Lazaro et al. 2019, **IFPEN**) significantly **improves** the predictions.



$$H_{H_2} = \frac{P * \varphi_{H_2} * y_{H_2}}{x_{H_2} * Poy_{H_2}(P, T)} \quad \text{with: } Poy_{H_2}(P, T) = \exp\left(\vartheta_{H_2}^{\infty} \frac{P - p^{sat}}{RT}\right)$$

$$x_{H_2} = \frac{P * \varphi_{H_2} * y_{H_2}}{H_{H_2} * Poy_{H_2}(P, T)}$$

P: Total pressure

$\varphi_{H_2}(\mathbf{T}, \mathbf{P})$: fugacity coefficient of H_2 in the vapor phase

y_{H_2} : H_2 content in the vapor phase

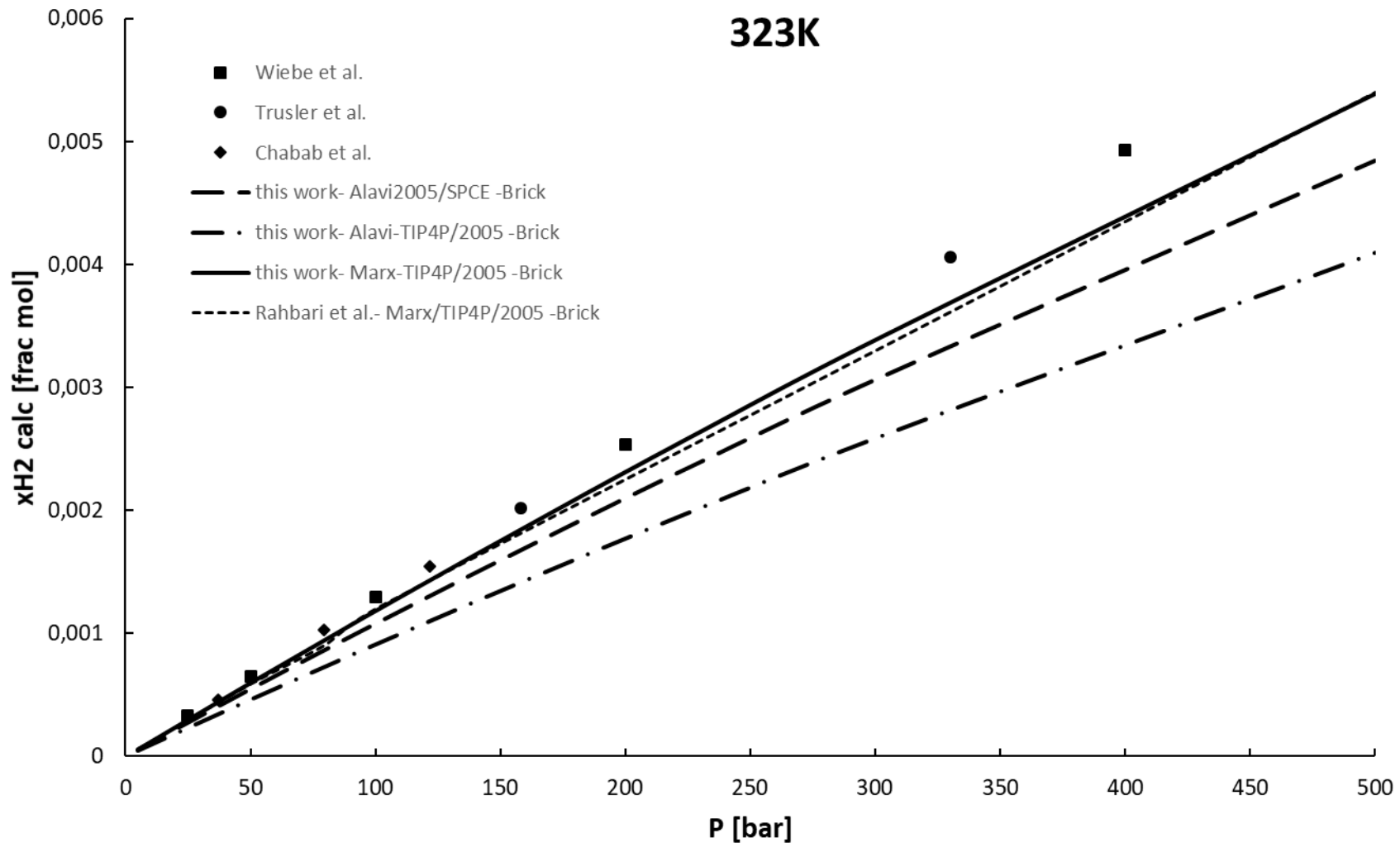
$Poy_{H_2}(\mathbf{T}, \mathbf{P})$: *Poynting factor*

$\vartheta_{H_2}^{\infty}$: partial molar volume of H_2 at infinite dilution

$\vartheta_{H_2}^{\infty} = f(\mathbf{T})$, It is assumed that $\vartheta_{H_2}^{\infty} \neq f(P)$

- From the literature (available only at $T=298.15^\circ \text{ C}$ and $P=1 \text{ bar}$)
- From molecular simulation





Thermodynamics modeling of the H₂ + H₂O + NaCl system



I) Symmetric approach (phi-phi)

Same Equation of State (EoS) for each phase

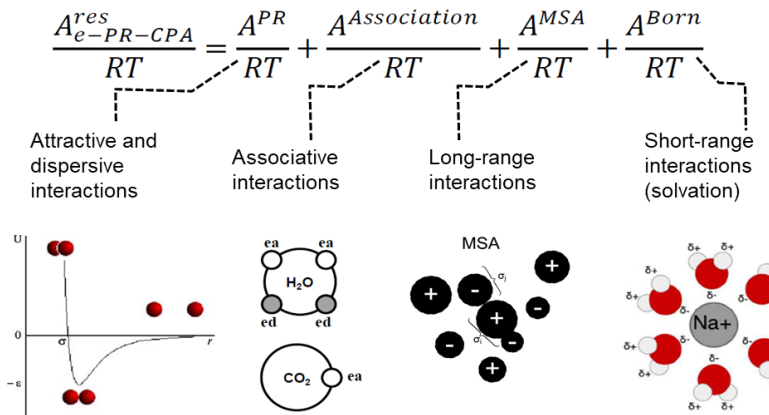
$$x_i \Phi_i^{Liq} = y_i \Phi_i^{vap}$$

1) Soreide and Whitson (SW) EoS

- Peng-Robinson EoS with different BIPs (T and salinity dependent) for liquid and gas phases and a specific alpha-function for brine.
- Recent parameters from [Chabab et al. 2021](#)

2) e-PR-CPA EoS

(ref : [Chabab et al., 2019](#))



II) Asymmetric approach (gamma-phi)

3) Using Henry's constant

$$x_i^{aq} \gamma_i^{aq} H_i^g(T, P^{sat}) \exp\left(v_i^\infty \frac{P - P^{sat}}{RT}\right) = y_i^g \phi_i^g P$$

Liquid
Gas

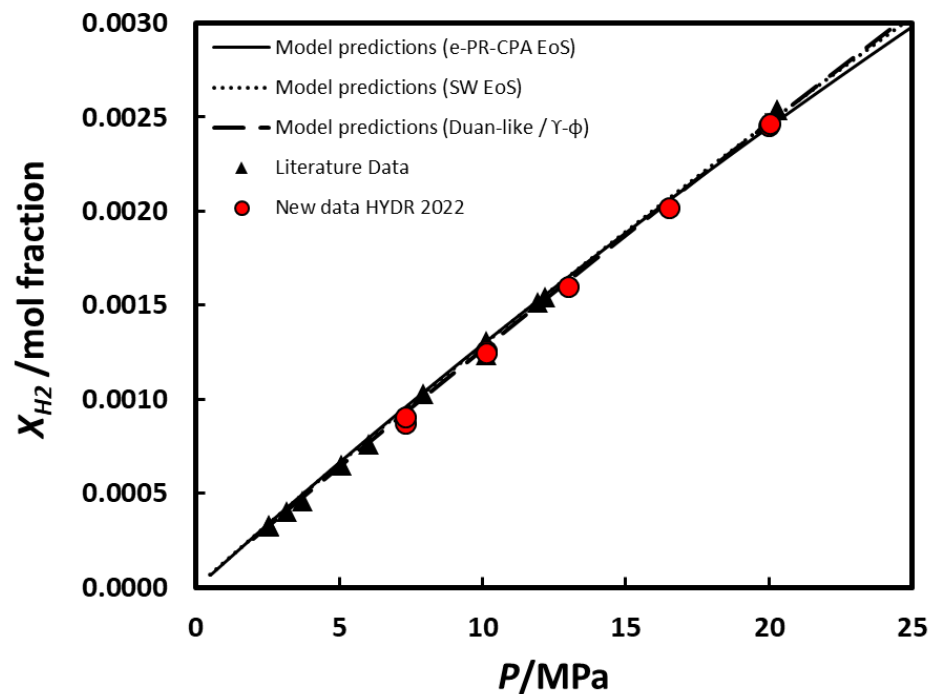
4) Duan-type model

$$\mu_i^{l(0)} + RT \ln(\gamma_i) + RT \ln(x_i) = \mu_i^{v(0)} + RT \ln(y_i P) + RT \ln(\phi_i)$$

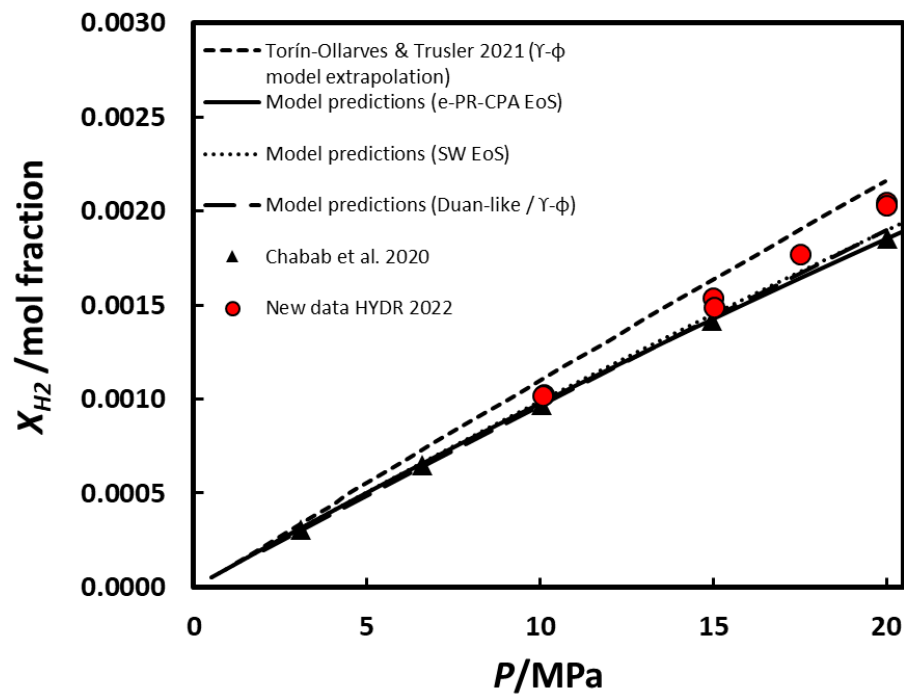
Liquid
Gas

$T = 323.15 \text{ K}$

$H_2 + H_2O$



$H_2 + H_2O + 1m \text{ NaCl}$

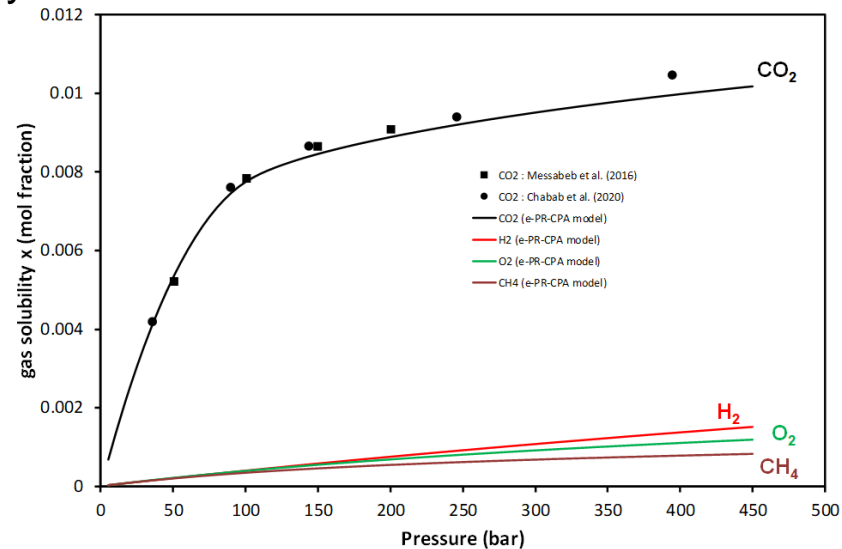
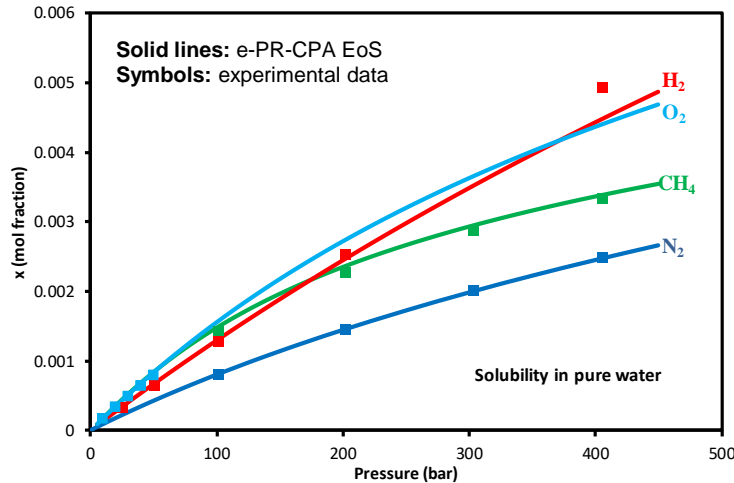


1) Salting-out effect of CH₄, N₂, O₂, and H₂ in 1m NaCl brine

	CH ₄	O ₂	N ₂	H ₂
$100 * (1 - x_{in\ brine} / x_{in\ water})$	25.35	25.38	25.24	17.18 (This work) 12.25 (Torín & Trusler 2021) 24.28 (Chabab et al. 2020)

2) Gas solubility dependencies:

- Intermolecular forces (HB, e.g. CO₂)
- Coulombic interactions
- Molecule size
- Polarizability



(To go deeper, see **Battino, R., & Seybold, P. G. (2011). The O₂/N₂ Ratio Gas Solubility Mystery.**)

Summary

- Importance of thermophysical properties for UHS
- Impact of density and chemical potential on solubility prediction (MC simulation)
- Different approaches for the calculation of solubility
- Predictive capacity of MS
- Salting-out effect
- Gas solubility dependencies

Upcoming work

- Mixed-gas co-solubility (cushion gas, underground bio-methanation, etc.)
- H₂ diffusivity in brine
- Interfacial tension of H₂/mixed gas with brine (short/medium term)
- Impact of clay (long term perspective)





Thank you for your attention!

Acknowledgements



LaTEP lab (UPPA)

Pierre CÉZAC
Marie POULAIN
Marion DUCOUSSO

LFCR lab (UPPA)

Guillaume GALLIERO
Hai HOANG
Halla KERKACHE

External collaborators

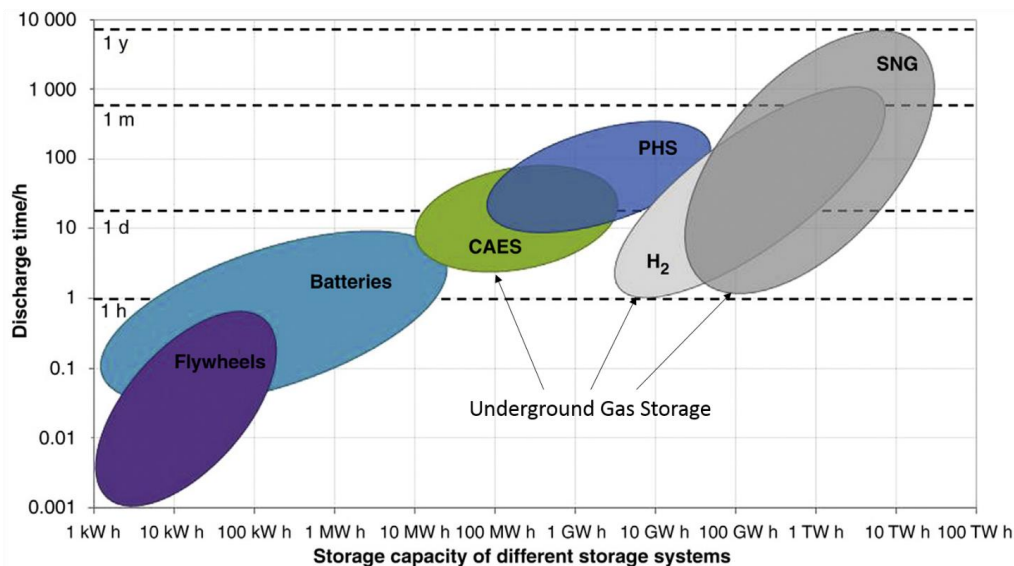
Olivier BAUDOIN (ProSim)
Colleagues from IFPEN
Christophe COQUELET (Mines)



Additional slides

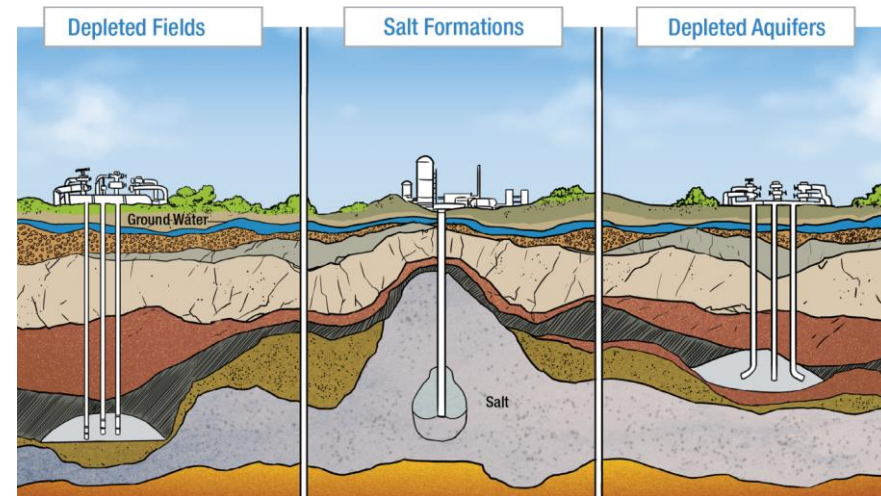


Overview of the different types of energy storage



Ref : Tichler & Bauer (2016). Power-to-Gas. In Storing Energy.

Principal types of underground gas storage



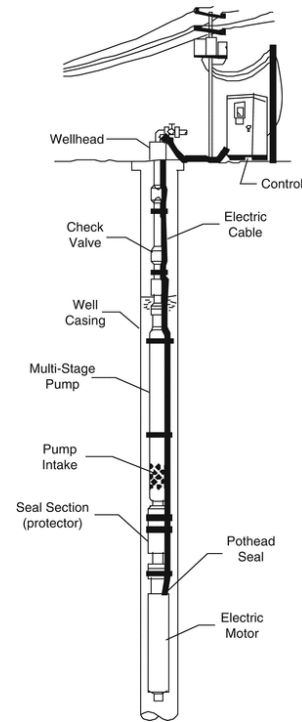
Ref : J.I.T. Force (2016), Underground natural gas storage: Integrity and safe operations



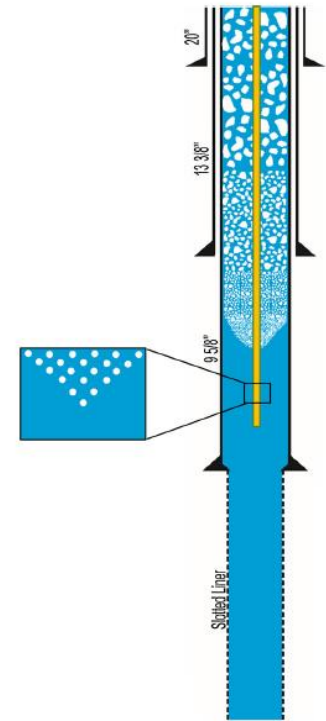
Effect of degassing in geothermal processes:

- Reducing the process efficiency
- pH change : salt (e.g., calcite- CaCO_3) scaling
- Causing undesired GHG emissions

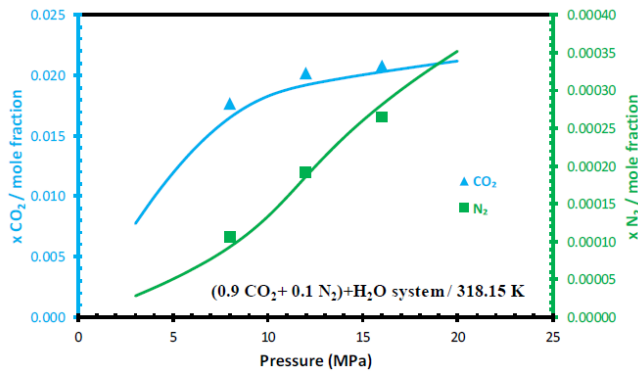
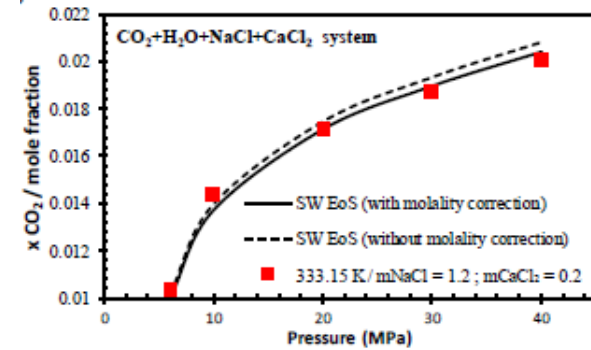
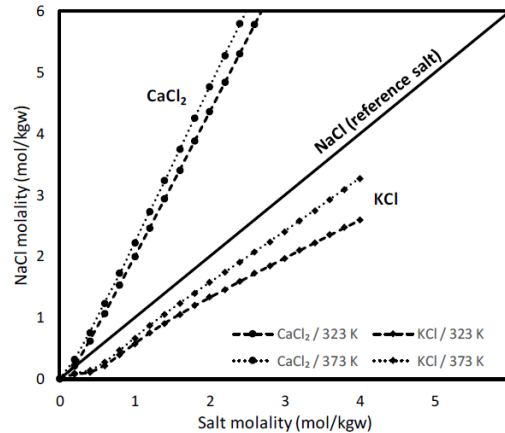
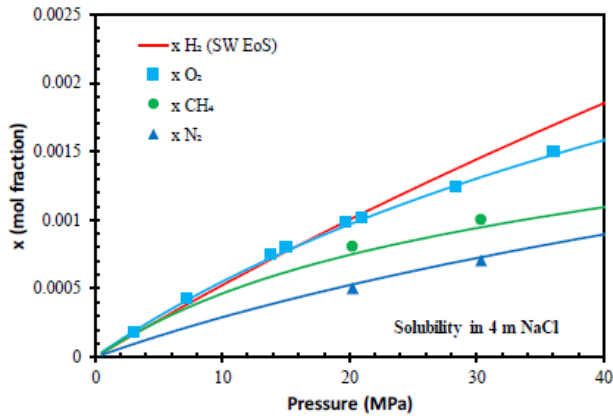
- **Gas breakout depth**
- **Working pressure in surface facilities**



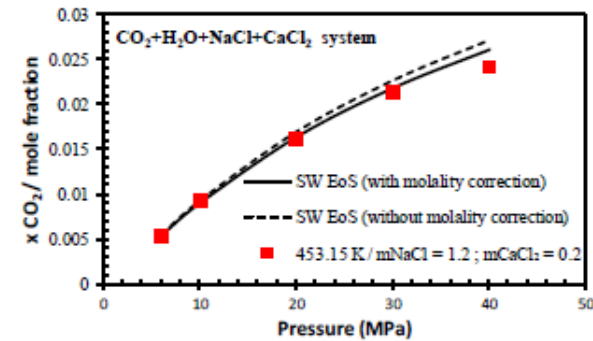
Submersible pump



First gas bubble formation

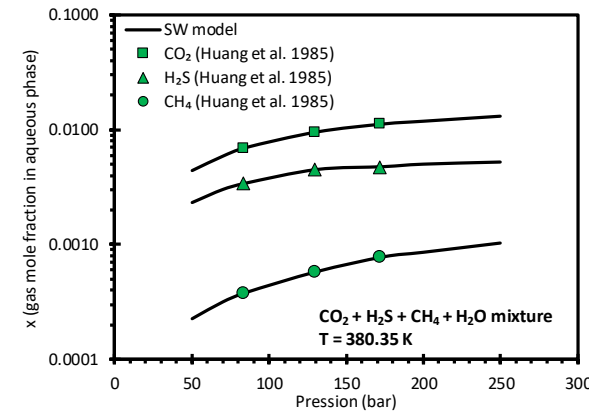


Model : SW EoS with **new** parameters and different salts



- ✓ Duhring lines of equal Gas solubility in different brines
- ✓ Mutual Solubilities of Gas-Brine (Single or Mixed Salts)
- ✓ Mixed-gas cosolubility

Ref : 1) Chabab, S et al. (2021). *Energies*, 14, 5239.
 2) Chabab, S et al. (2022). EGC 2022, Berlin.



Prediction of :

- ✓ Bubble-Point Pressure and
- ✓ GHG Emission Rate (g-eqCO₂/kWh) in the Upper Rhine Graben Geothermal Sites

Selected models :

- ❖ Phase equilibria : EoS (Sørense and Whitson) with new parameters
- ❖ GLR conversion : GERG-2008 for gas, Al Ghafri's correlation for brine

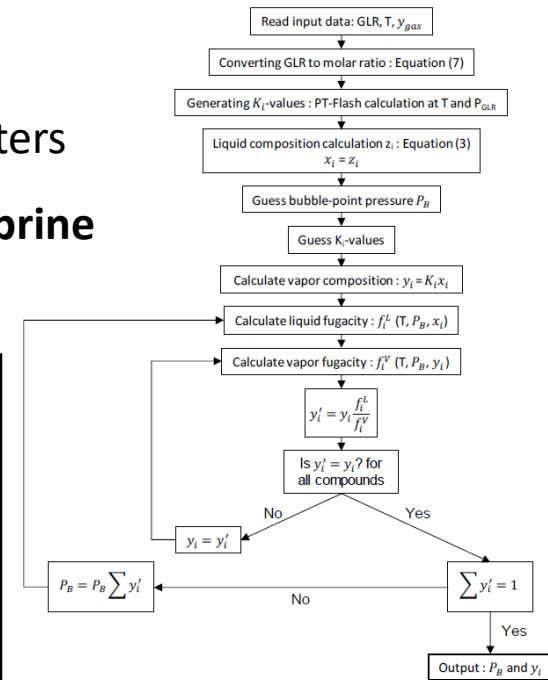
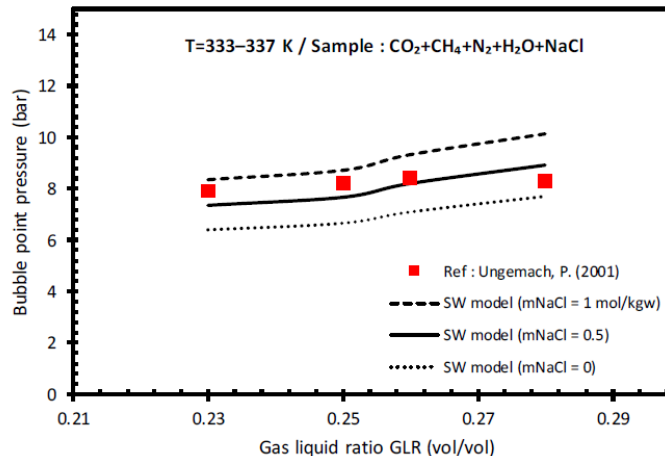
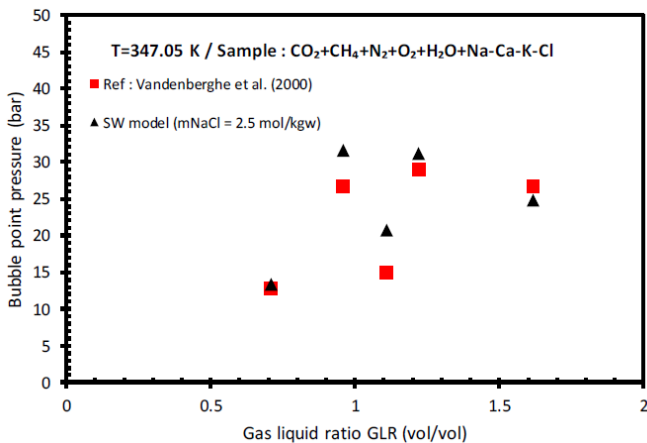


Figure 2. Algorithm for calculating the bubble point pressure of geothermal fluids.

Chabab, S et al. (2021). Energies, 14, 5239.